

FLOMEKO 2019

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Flow Measurement Turn Down Analysis for DP Flow Meter using Multiple Multivariable Transmitters

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Oral Session S8.9: Flow Metering Technology

Room5

FLOMEKO2019

Portugal, Lisbon, LNEC

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Outline

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2: The motivation of this research

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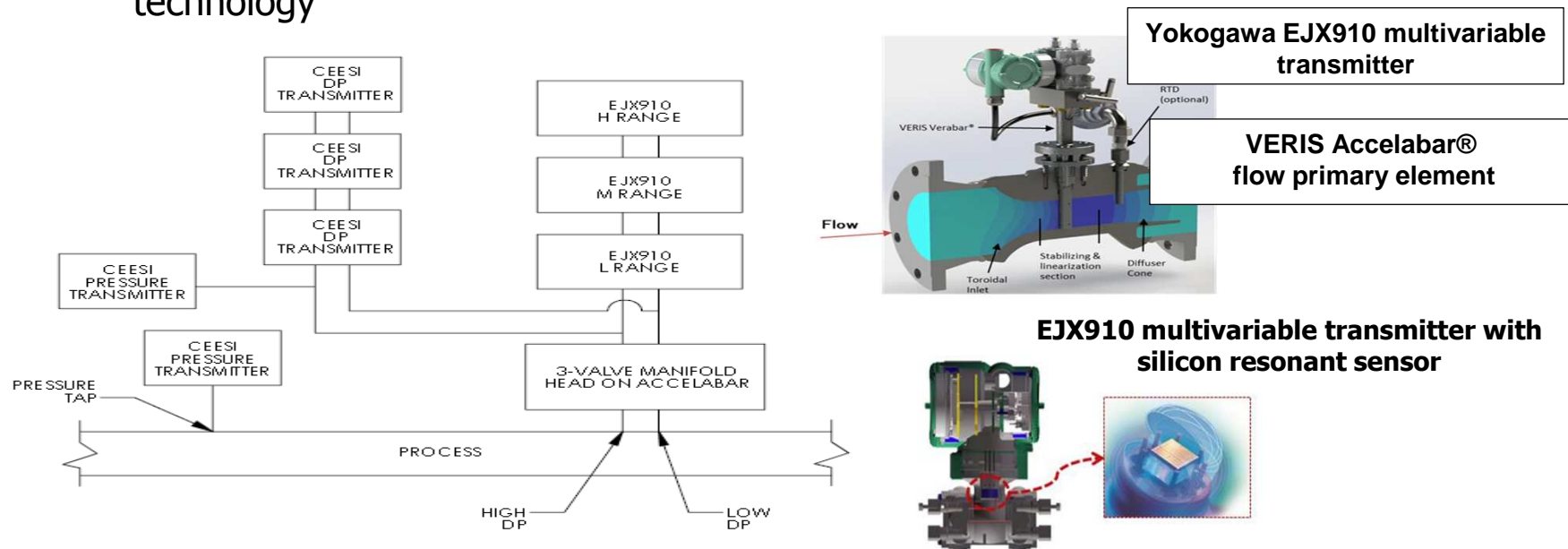
5. Uncertainty analysis at 2.2 inH₂O point

6. DP measurement contribution for flow measurement

7. CONCLUSION

1. INTRODUCTION: Differential pressure (DP) flow meter calibration at CEESI, reported at ISFFM2018

- ❖ We reported at ISFFM2018 that we performed a DP flow meter calibration to determine the combined system accuracy at the CEESI NIST traceable air laboratory located at Nunn, Colorado, USA
 - 4" VERIS Accelabar® flow primary element based on averaging pitot tube technology
 - Combines a unique toroidal nozzle design with the VERIS Verabar® averaging pitot tube
 - Yokogawa EJX® Series multivariable transmitter EJX910 H range (2000inH2O) and M range (400inH2O)
 - Designed with multi-sensing capabilities using built-in silicon resonant sensor technology



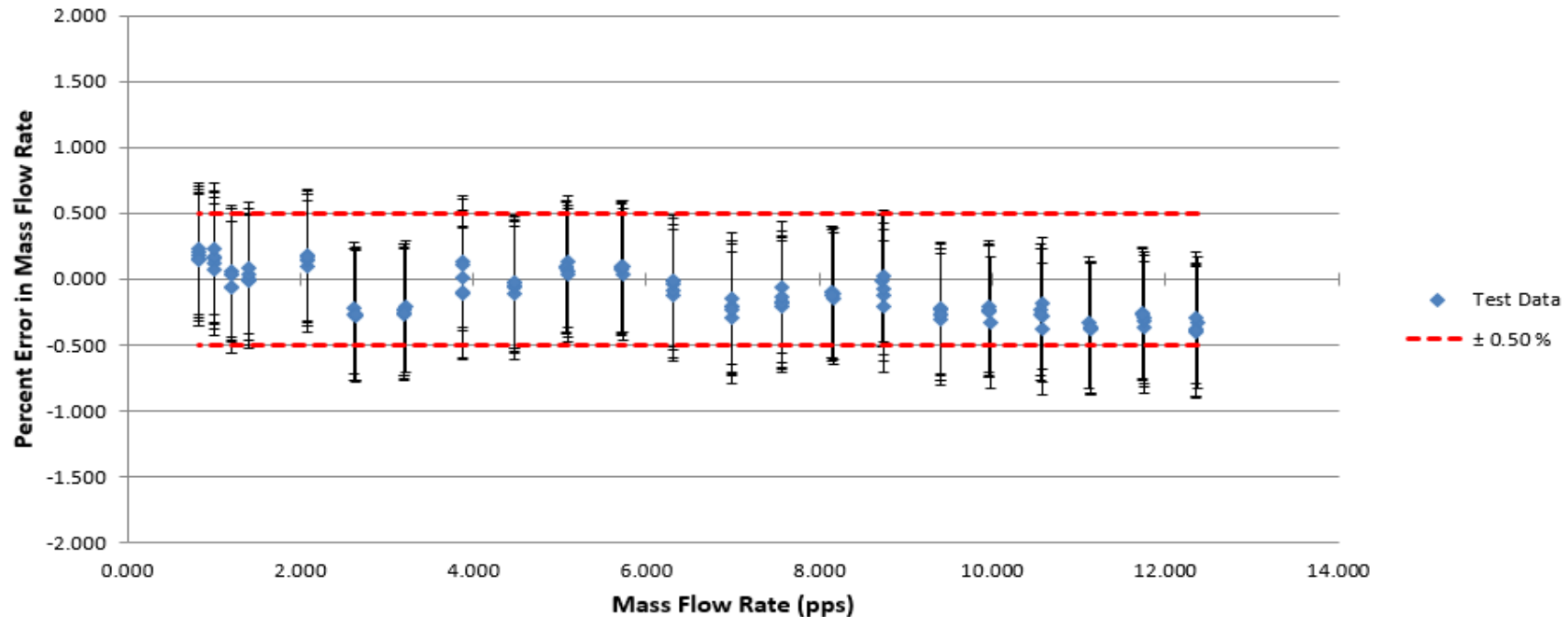
❖ 1. INTRODUCTION: Flow measurement result using single multivariable transmitter, reported at ISFFM2018

- ❖ For FLOMEKO2019, we focus below
- ❖ Flow rate outputs of the EJX910 transmitters were compared to CEESI flow rates determined by CEESI's NIST traceable sonic nozzles
- ❖ VERIS Accelabar® flow coefficient (K) value was corrected from EJX910 flow data to match CEESI flow data
 - The best performance was achieved during the 800 psia air tests
 - The result obtained using single EJX910 H range (2000inH₂O) was reported at ISFFM2018
 - The combined linearity of VERIS Accelabar® flow primary element and Yokogawa EJX910 DP measurement was 0.5% with 15:1 turndown

1. INTRODUCTION: Flow measurement result using single multivariable transmitter, reported at ISFFM2018

- Achieved accuracy 0.5% with 15:1 turndown
 - EJX910 H range with the 4" VERIS Accelabar®

4 Inch Accelabar, 800 psia, H Range EJX910
Combined Accelabar and Transmitter Error, Calibrated Flow Coefficient
Flow Coefficient corrected to match CEESI mass flow rate



❖ 2. The motivation of this research

- ❖ EJX910 has also L range (DP: 40inH₂O) transmitter and capability of using for low flow rate measurement
 - We show that adding L range transmitter with H range transmitter, flow measurement turndown will be increased beyond 15:1 until 20:1
- ❖ We show that EJX910 has an advantage of low DP measurement under high static pressure (SP) condition

→ 2. The motivation of this research

→ Flow rate equation at CEESI flow test

$$q_m = \frac{\pi}{4} K \varepsilon D^2 \sqrt{2 \Delta P \rho_f} \quad (1)$$

Where

K stands for flow coefficient

ε stands for expansibility

D stands for diameter of the conduit

ΔP stands for DP

ρ_f stands for density

→ Flow turndown 20:1 flow rate point

	maximum	15:1 flowrate from maximum	20:1 flow rate from maximum
Flow rate (lb/sec)	12.4	0.82	0.62
Dp (InH2O)	890	3.9	2.2

→ Analyze 20:1 flow point uncertainty

→ Confirm if flow measurement turndown will be increased beyond 0.5% 15:1 until 20:1 in case of adding L range transmitter

❖ 3. Combined flow uncertainty: The uncertainty assumption of Flow Primary element and the density

❖ Combined flow uncertainty

$$\frac{\delta q_m}{q_m} = \sqrt{\left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 + \left(\frac{\partial \Delta P}{2\Delta P}\right)^2 + \left(\frac{\partial \rho}{2\rho}\right)^2} \quad (7)$$

❖ The uncertainty contribution of Flow Primary element VERIS Accelabar®

$$Uncert_{pe_as} = \left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 = (0.5\%)^2 \quad (10)$$

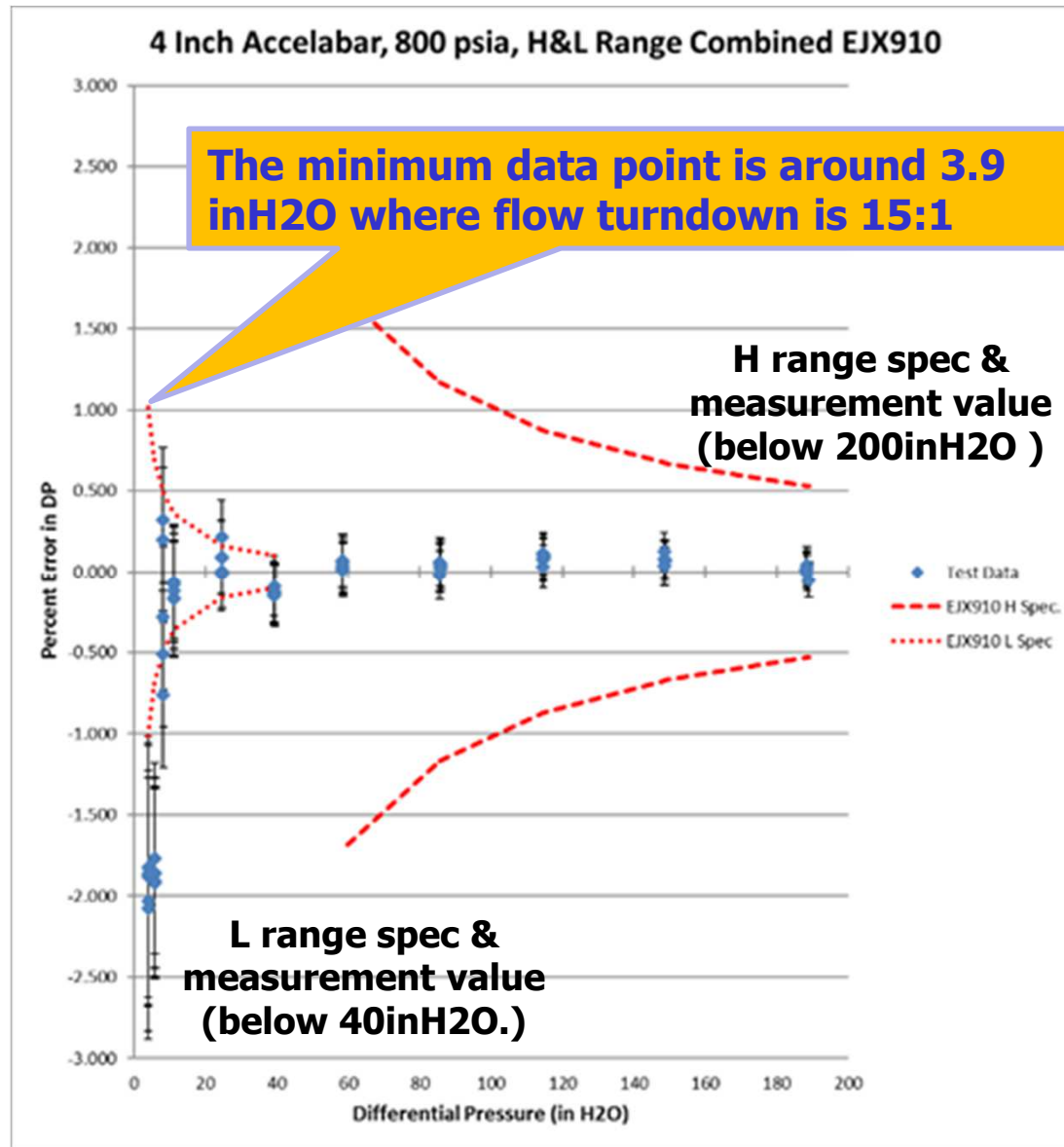
❖ Assume that VERIS Accelabar® flow uncertainty contribution is 0.5% with 20:1 turndown derived by previous experiments

❖ The uncertainty contribution of the density

$$Uncert_{\rho_as} = \left(\frac{\partial \rho}{2\rho}\right)^2 = (0.05\%)^2 \quad (13)$$

❖ Assume by current EJX910 specification
– Density uncertainty less than 0.1%

4. DP uncertainty analysis : L & H range DP comparison with CEESI master meter



- The EJX910 L range data difference between the EJX910 H range and CEESI master meter at the point is around 2%
- The EJX910 uncertainty calculated by general specification is around 1%
- The CEESI master meter uncertainty is 0.8%
- The uncertainty of EJX910 and the reference CEESI master meter at the point is relatively bigger than the difference

❖ 5. Uncertainty analysis at 2.2 inH2O point: DP reference accuracy influence

❖ Combined flow uncertainty

$$\frac{\delta q_m}{q_m} = \sqrt{\left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 + \left(\frac{\partial \Delta P}{2\Delta P}\right)^2 + \left(\frac{\partial \rho}{2\rho}\right)^2} \quad (7)$$

❖ From reference accuracy defined as $\pm 0.04\%$ of span

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{ref} = 0.04\% \times \frac{40 \text{ inH2O}}{2.2 \text{ inH2O}} = 0.7\% \quad (15)$$

❖ From L range EJX910 test data at the factory

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{ref_as} = 0.005\% \times \frac{40 \text{ inH2O}}{2.2 \text{ inH2O}} = 0.09\% \quad (16)$$

5. Uncertainty analysis at 2.2 inH2O point: SP span effects influence

Combined flow uncertainty

$$\frac{\delta q_m}{q_m} = \sqrt{\left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 + \left(\frac{\partial \Delta P}{2\Delta P}\right)^2 + \left(\frac{\partial \rho}{2\rho}\right)^2} \quad (7)$$

From SP span effects per 6.9 MPa (1000 psi) change defined as $\pm 0.075\%$ of span

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{span} = 0.075\% \times \frac{800 \text{ psia}}{1000 \text{ psia}} \times \frac{40 \text{ inH2O}}{2.2 \text{ inH2O}} = 1.1\% \quad (17)$$

From L range EJX910 test data at the factory

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{span_{as}} = 0.01\% \times \frac{800 \text{ psia}}{1000 \text{ psia}} \times \frac{40 \text{ inH2O}}{2.2 \text{ inH2O}} = 0.15\% \quad (18)$$

❖ 5. Uncertainty analysis at 2.2 inH2O point: Assumed uncertainty at 2.2 inH2O point

❖ Combined flow uncertainty

$$\frac{\delta q_m}{q_m} = \sqrt{\left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 + \left(\frac{\partial \Delta P}{2\Delta P}\right)^2 + \left(\frac{\partial \rho}{2\rho}\right)^2} \quad (7)$$

❖ From Equation 16 (DP reference accuracy influence) and 18 (SP span effects influence)

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{as} = \left(\frac{\partial \Delta P}{\Delta P}\right)_{ref_as} + \left(\frac{\partial \Delta P}{\Delta P}\right)_{span_as} = 0.09\% + 0.15\% = 0.24\% \quad (19)$$

❖ 5. Uncertainty analysis at 2.2 inH2O point: Assumed uncertainty at 2.2 inH2O point

❖ Combined flow uncertainty

$$\frac{\delta q_m}{q_m} = \sqrt{\left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 + \left(\frac{\partial \Delta P}{2\Delta P}\right)^2 + \left(\frac{\partial \rho}{2\rho}\right)^2} \quad (7)$$

❖ DP uncertainty at 2.2 inH2O point (flow turndown 20:1) from equation 19

$$\text{Uncert}_{dp_{as}} = \left\{ \left(\frac{\partial \Delta P}{2\Delta P} \right)^2 \right\}_{as} = \left(\frac{1}{2} \times \left(\frac{\partial \Delta P}{\Delta P} \right)_{as} \right)^2 = \left(\frac{1}{2} \times 0.24\% \right)^2 = (0.12\%)^2 \quad (20)$$

→ 5. Combined flow uncertainty: Extending flow turn down to 20:1

→ Combined flow uncertainty

$$\frac{\delta q_m}{q_m} = \sqrt{\left(\frac{\partial K}{K}\right)^2 + \left(\frac{\partial \varepsilon}{\varepsilon}\right)^2 + \left(\frac{2\partial D}{D}\right)^2 + \left(\frac{\partial \Delta P}{2\Delta P}\right)^2 + \left(\frac{\partial \rho}{2\rho}\right)^2} \quad (7)$$

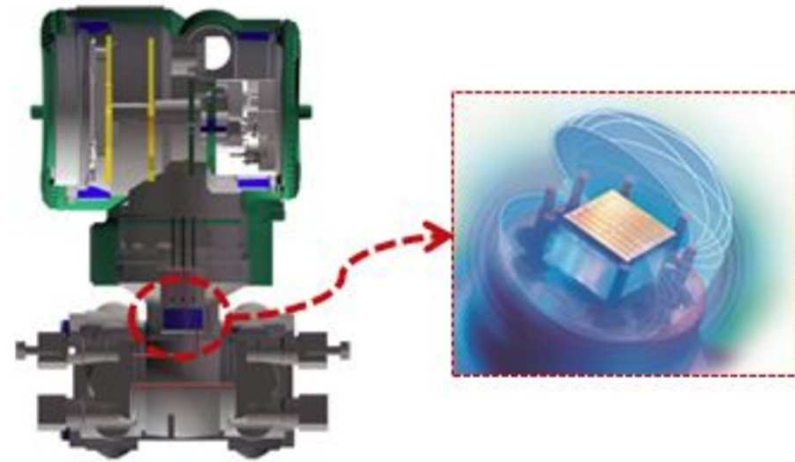
$$\left(\frac{\delta q_m}{q_m}\right)_{as} =$$

$$\begin{aligned} & \sqrt{(Uncert_{pe_as} + Uncert_{\rho_as} + Uncert_{dp_as})} = \\ & \sqrt{((0.5\%)^2 + (0.05\%)^2 + (0.12\%)^2)} = \\ & \sqrt{(0.25\% + 0.0025\% + 0.0144\%)} = \sqrt{0.2669} = \\ & 0.52\% \end{aligned} \quad (21)$$

→ 0.5 % with flow turn down 20:1 will be achieved using L range transmitter in addition to H range under CEESI test condition

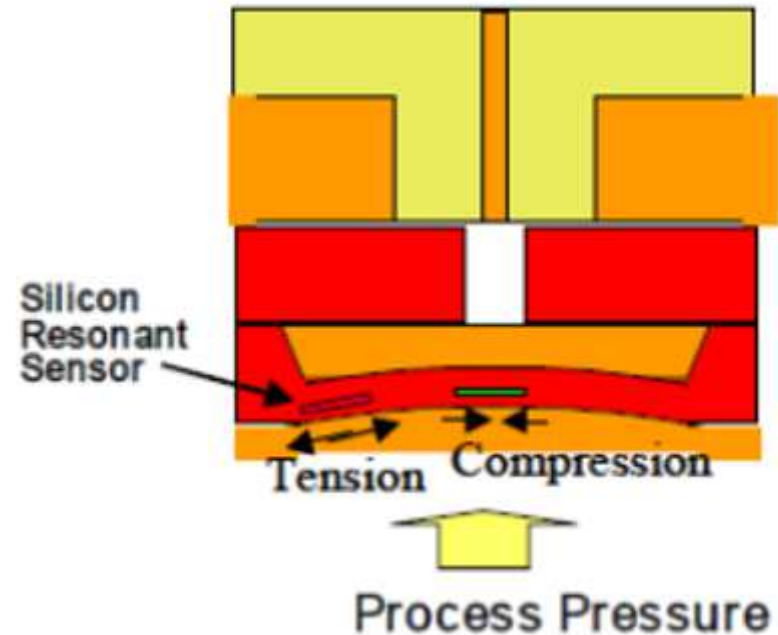
❖ 6. DP measurement contribution for flow measurement

- ❖ The EJX910 is designed with multi-sensing capabilities using built-in silicon resonant sensor technology
- ❖ The pressure sensor based on advanced silicon resonant sensor structure contributes to the flow measurement performance which realizes uncertainty 0.5% turn down 20:1 by multiple multivariable transmitters



❖ 6. DP measurement contribution for flow measurement: Pressure sensor structure

- ❖ Two resonators are incorporated into one sensor tip inside EJX910 using MEMS technology at the location of the silicon diaphragms
- ❖ Two resonators are located where tensile strain and compressive strain occur
- ❖ SP is simultaneously measured along with the DP by this one sensor tip



❖ 6. DP measurement contribution for flow measurement: Pressure sensor signal

❖ Changes (Δf^2) in resonance frequencies f_1 and f_2 of the two resonators due to the pressure

$$\Delta f_1^2 = \Delta f_{01}^2 \cdot G_{f1} (+\varepsilon_{dp1} + \varepsilon_{sp1}) \quad (22)$$

$$\Delta f_2^2 = \Delta f_{02}^2 \cdot G_{f2} (-\varepsilon_{dp2} + \varepsilon_{sp2}) \quad (23)$$

where

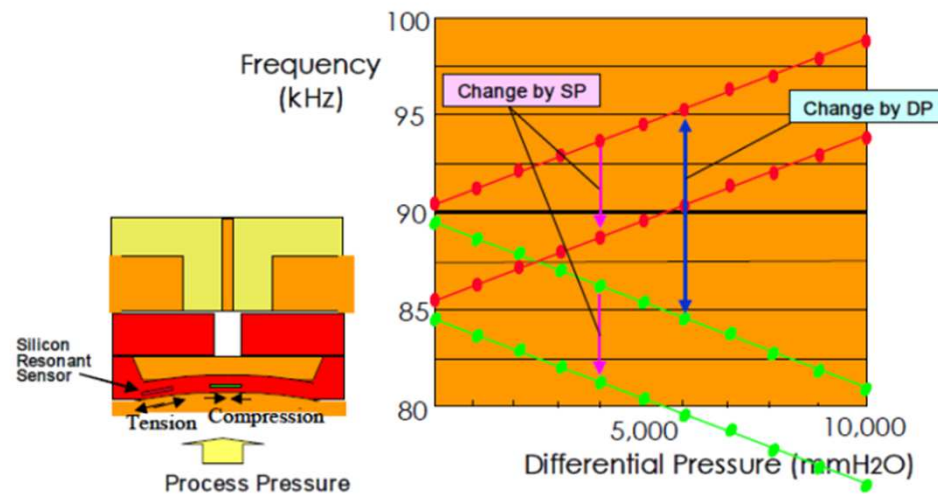
f_0 stands for the resonance frequency when the tensile force is zero

G_f stands for the squared sensitivity of the resonator ($=0.2366 \cdot (1/h)^2$)

h stands for thickness of the resonator

ε_{dp} stands for change in the tensile force due to DP

ε_{sp} stands for change in the tensile force due to SP



❖ 6. DP measurement contribution for flow measurement: Pressure sensor signal

❖ DP and SP change from equation 22 and 23

$$\Delta DP = \Delta f_1^2 - a \cdot \Delta f_2^2 \quad (24)$$

$$\Delta SP = \Delta f_1^2 + b \cdot \Delta f_2^2 \quad (25)$$

where

ΔDP stands for DP change

ΔSP stands for SP change

- ❖ DP and SP signals can be calculated by previously determining each coefficient from actual measured appropriate data
- ❖ EJX910 dynamically & continuously minimize the effect of SP fluctuation inside the transmitter

❖ 6. DP measurement contribution for flow measurement: Pressure sensor signal

❖ Provides precise DP measurement under real conditions which is explained

– in equation (15): DP reference accuracy influence

❖ From reference accuracy defined as $\pm 0.04\%$ of span

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{ref} = 0.04\% \times \frac{40 \text{ inH}_2\text{O}}{2.2 \text{ inH}_2\text{O}} = 0.7\% \quad (15)$$

❖ From L range EJX910 test data at the factory

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{ref_as} = 0.005\% \times \frac{40 \text{ inH}_2\text{O}}{2.2 \text{ inH}_2\text{O}} = 0.09\% \quad (16)$$

– in equation (18): SP span effects influence

❖ From SP span effects per 6.9 MPa (1000 psi) change defined as $\pm 0.075\%$ of span

$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{span} = 0.075\% \times \frac{800 \text{ psia}}{1000 \text{ psia}} \times \frac{40 \text{ inH}_2\text{O}}{2.2 \text{ inH}_2\text{O}} = 1.1\% \quad (17)$$

❖ From L range EJX910 test data at the factory

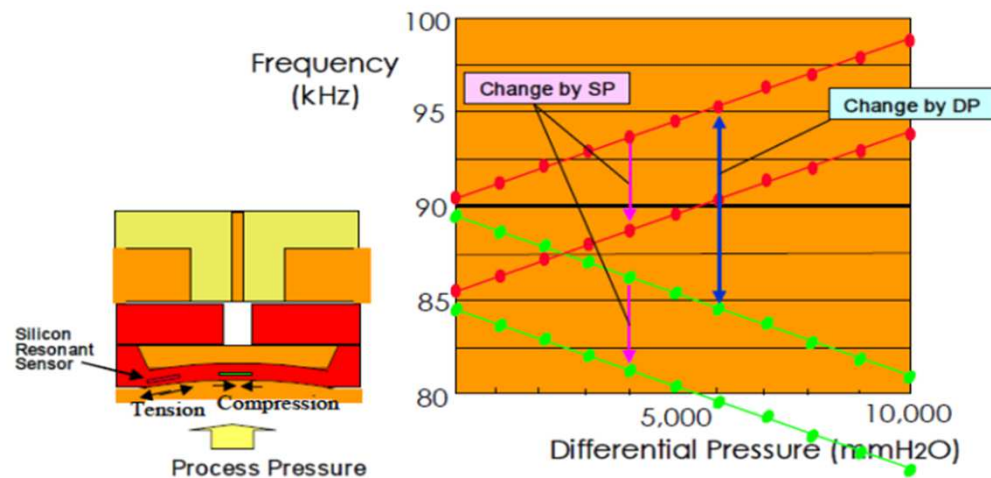
$$\left(\frac{\partial \Delta P}{\Delta P}\right)_{span_as} = 0.01\% \times \frac{800 \text{ psia}}{1000 \text{ psia}} \times \frac{40 \text{ inH}_2\text{O}}{2.2 \text{ inH}_2\text{O}} = 0.15\% \quad (18)$$

❖ 6. DP measurement contribution for flow measurement: Pressure sensor characteristics

- ❖ a) EJX910 silicon resonant sensor is made of single crystal which is tetrahedral structure with strong bonding. It reacts ideal elastic deformation from outside force
- ❖ b) EJX910 pressure whole range measurement is conducted under elastic deformation state.
 - The deformation is proportional and uniform
 - The hysteresis is small
 - The two resonators deformation precisely match the theoretical Equation (22) and (23)
- ❖ c) Two resonators are incorporated into one sensor tip and the compensations (24) and (25) are achieved precisely
$$\Delta DP = \Delta f_1^2 - a \cdot \Delta f_2^2 \quad (24)$$
$$\Delta SP = \Delta f_1^2 + b \cdot \Delta f_2^2 \quad (25)$$
- ❖ d) The silicon resonant sensor is inside the vacuum cavity and the resonance is robust from outside disturbance

❖ 6. DP measurement contribution for flow measurement: Low DP measurement under high SP condition

- ❖ The two resonators signals are influenced by the DP and the SP
 - The resonators frequency shifts according to the DP and the SP changes
 - Keeping two resonators frequency relation
- ❖ The changes are proportional and uniform and the hysteresis is small
 - SP compensations of DP signal for whole ranges are achieved precisely
 - The uncertainty of the DP is small even at the condition of low DP under high SP
- ❖ EJX910 has an advantage of low DP measurement under high SP condition



→ 7. CONCLUSION

- Combined DP flow meter VERIS Accelabar® flow primary element and Yokogawa EJX910 multivariable L range transmitter are analyzed
 - Adding EJX910 L range transmitter with H range transmitter, combined flow measurement turndown will be increased beyond 15:1 until 20:1 under 0.5% linearity with reference flow rate.
- EJX910 is designed with multi-sensing capabilities using built-in silicon resonant sensor technology
 - EJX910 dynamically & continuously minimizes the effect of SP fluctuation with two resonators incorporated into one sensor tip
 - Provides precise DP measurement under real conditions
 - EJX910 has an advantage of low DP measurement under high SP condition with built-in silicon resonant sensor technology
- These indicate the latest progress of DP flow meter technology
 - DP flow meter has still big potential for use in industry widely

❖ Thank you for your kind attention.